





# **East Sussex County Council Transport and Environment**

## Bexhill to Hastings Link Road G05 Decoy Pond South Underbridge Approval in Principle

Doc. Ref: B1297000-PH2/1600.06a/0021

Revision 0

September 2012



B1297000

### Document control sheet

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Bexhill to Hastings Link Road

Client:

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Transport and Environment

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## **Revision Summary**

Client:

East Sussex County Council Bexhill to Hastings Link Road

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Transport and Environment

Job No:

B1297000

Project: Document Title:

G05 Decoy Pond South Underbridge

**AIP** 

REVISION / DATE	COMMENT
Rev 0 14/09/12	Amended to incorporate TAA comments raised on Phase 1 AIP ref. JB-B1297000-PH1/1600.06a/0021 (rev 0)  Approach embankment ground treatment proposals added.  Steel/timber bridleway parapet proposed.
	Steel deck waterproofing Departure added.  Geotechnical information updated.

### 1. HIGHWAY DETAILS

### 1.1 Type of highway

Greenway - 3.65m wide shared equestrian, pedestrian, cyclist and Environment Agency maintenance access track with 0.6m wide margins either side.

### 1.2 Permitted traffic speed

Over: N/A - No public vehicular access.

Under: N/A

### 1.3 Existing restrictions

The structure spans a Main River for which the Environment Agency bears responsibility.

### 2. SITE DETAILS

### 2.1 Obstacles crossed

An un-named Environment Agency designated Main River with a square top of bank to top of bank width of approximately 12.0m.

### 3. PROPOSED STRUCTURE

### 3.1 Description of structure

The underbridge is located at OS grid reference 576765.720E, 110826.243N. It is approximately 40m to the south of the proposed Bexhill to Hasting Link Road Decoy Pond Underbridge. The structure carries the proposed Greenway over the stream feeding Decoy Pond..

The structure is a proprietary single span painted steel bridge supported on reinforced concrete abutments.

### 3.2 Structural type

Simply supported single-span main and secondary steel girders supporting stiffened steel decking plates and metal parapets. Main girders are located on bearings supported on reinforced concrete abutments.

The wingwalls are both cantilevered from the bankseats and free-standing gravity cantilever retaining walls with partially debonded dowel connections to mitigate differential settlement between structural elements.

Approach embankments and earthworks local to the structure are supported on controlled modulus column ground treatment to control differential settlement between earthworks, bridge abutments and free-standing wing walls. The ground treatment will be undertaken in advance of the structural foundation construction.

### 3.3 Foundation type

Reinforced concrete abutment founded on bored, cast in-situ reinforced concrete piles.

### 3.4 Span arrangements

Square span (between bearing centrelines): 17.2m Skew angle: 0.0 degrees

### 3.5 Articulation arrangements

Bearings will be elastomeric with longitudinal fixity provided on one abutment.

Expansion joints will consist of steel cover plates.

### 3.6 Types of road restraint systems

1.8m high bridleway parapets. Steel parapet posts with timber rails and timber infill to be designed for Class 3 post and rail loading and Type C infill loading to BS7818.

### 3.7 Proposed arrangements for maintenance and inspection

### 3.7.1 Traffic management

N/A

### 3.7.2 Access

A minimum 2.0m wide set back from top of bank will be provided in front of bearing shelves. A minimum 1.5m clear headroom will be provided from the maintenance area in front of abutments to the deck soffit between main girders. Bearing shelves will be a minimum of 600mm above the adjacent maintenance platform level.

Inspection and maintenance of the abutments and wing walls can be carried out at ground level or from a ladder or temporary scaffold for upper areas.

Foundations will not be visible or accessible for inspection.

The deck soffit and outer parapet faces can be accessed by scaffold/ladder from the river banks or from the track above using a small underbridge unit.

Bearings at abutments will be set on plinths as necessary to provide 300mm minimum clearance between the beam soffit and bearing shelves for inspection and maintenance purposes. Jacking points will be provided between main beams for bearing replacement. The bridge will be designed to carry its full design load during bearing replacement.

## 3.8.1 Materials and finishes – relating to new construction only and not to elements of existing structure retained in new works

Concrete	Element		Limiting Exposure Class	
C32/40	Piles		DC-3z. Note A	
Note A			refore Design Chemical Class for inical Summary Sheet for detail.	
C40/50	Substructure, buried Substructure, exposed abutment		DC1 XC3/4, XF3	
Reinforcement		Grade B500B or grade :2005	e B500C deformed bars to BS4449	
		Dowels to be stainless steel : Strength Grade 500, material designation 1.4436 complying with BS		

6744:2001 +A2:2009.

Structural steelwork All structural steelwork to BS EN 10025 Grade S355J2+N

or AdvanceS355J2 for rolled sections.

Bolts HSFG steel bolts to BS 4395 Part 1

Parapets 1.8m high bridleway parapet to BS 7818.

Parapet posts to be galvanised painted steel. Rails and

solid infill panels to be timber.

Backfill to abutments and

retaining walls

Class 6N/6P structural fill in accordance with DoT

Specification for Highway Works.

**Concrete Finishes** 

Hidden and buried surfaces

F1/U1

Exposed faces of abutment and

wing walls

F6 grooved patterned profiled finish / U2

### Protection

All accessible concrete surfaces greater than 150mm below finished ground level to receive waterproofing to below ground concrete surfaces in accordance with the SHW CI 2004.

All exposed concrete elements will receive anti-graffiti coating.

All structural steelwork shall be painted with an approved Type II (Inland, Difficult Access) paint system with a maintenance period of 20 years in accordance with DoT Specification for Highway Works.

Deck surfaces shall be coated with a suitable proprietary non-slip surfacing.

Parapet posts shall be galvanised steel painted with an approved Type IV paint system with a maintenance period of 20 years in accordance with the SHW.

Holly Green 14C39 Colour to BS 4800:1989 is proposed for all painted steelwork.

### 3.8.2 Sustainability issues

The materials and protective measures proposed are intended to maximise the durability of the structure and to minimise the requirement for future maintenance.

### 3.9 Risks and hazards considered

Standard construction methods are anticipated along with normally associated risks and hazards. The risks and hazards associated with the construction activities relating to these works will be identified by the appropriate method statements and safe working practices, to be completed prior to any construction taking place.

Risks associated with working at height and over water will be limited by maximising the amount of prefabrication of steelwork elements off-site.

### 3.10 Estimated cost of proposed structure together with other structural forms considered and the reasons for their rejection including comparative whole-life costs with dates of estimates.

The relative advantages, disadvantages and costs of various structural forms are discussed and appraised in Owen Williams reports No. 262701/012 'BHLR Structures Options Report' and No. 262701/060 'BHLR Structures Options Report – Addendum'.

### 3.11 Proposed arrangements for construction

3.11.1 Traffic management

N/A

3.11.2 Service diversions

N/A

3.11.3 Interface with existing structures

N/A

### 4. DESIGN CRITERIA

### 4.1 Live loading, Headroom

### 4.1.1 Loading relating to normal traffic under AW regulations and C&U regulations

3t Assessment Live Loading (ALL) in accordance with BD21/01, including wheel and axle loading, assuming Low Traffic Flow and Good Road Surface category.

### 4.1.2 Loading relating to General Order traffic under STGO regulations

Not required.

### 4.1.3 Footway or footbridge live loading

Foot/cycle track loading will be in accordance with BD 37/01 Cl 6.5.1 with the width of pedestrian area considered as the full width of deck between parapets ie 4.85m. In accordance with Cl 6.5.1 the pedestrian load intensity will be reduced by 15% in the 2m-3m width and 30% in the 3m-4.85m range. The applied load will taken as the average intensity.

4.1.4 Loading relating to Special Order Traffic, provision for exceptional abnormal loads or indivisible loads, including location of vehicle track on deck cross-section

Not required.

### 4.1.5 Any special loading not covered above

EA maintenance access vehicle – 24t tracked excavator (based on JCB JZ 255). Load factors to be as per BD37/01 HA loading. Impact factor = 1.2 due to extreme low speed.

Construction loading from 6t dumper (W1 = 7.5t, W2 = 3.0t, A1 = 2.4m) to be applied in accordance with BD21/01 Annex D.

Approach embankments founded on soft ground will be subjected to advance works ground treatment ie controlled modulus column installation, in advance of structural piling. Any residual lateral load or negative skin friction effects resulting from approach embankment loadings will be assessed and included in the design loadings for the bridge piled foundations.

Heavy or high load route requirements and arrangements being made to 4.1.6 preserve the route, including any provision for future heavier loads or future widening.

Not required.

#### 4.1.7 Minimum headroom provided

### From east platform:

- 1.54m to soffit of discrete main steel girders.
- 1.70m to soffit of deck between discrete girders.

### From west platform:

- 2.22m to soffit of discrete main steel girders.
- 2.38m to soffit of deck between discrete girders.

### From 100yr flood level+20%:

- 3.20m to soffit of discrete main steel girders.
- 4.20m to soffit of deck between discrete girders.

### Minimum headroom required:

- 1.05m to soffit of discrete main steel girders.
- 1.5m to soffit of deck between discrete girders.
- 0.6m free-board above 100yr flood level+20%

#### 4.1.8 Authorities consulted and any special conditions required

#### Special Requirement **Authority Consulted**

**Environment Agency** 

A minimum 2m margin on each bank and the soffit level to be set a

minimum 600mm above the predicted 1 in 100 year flood (+20%)

level.

24t tracked excavator access requirement with minimum width of

12ft.

British Horse Society

Non-slip deck surface.

**ESCC** 

Planning Condition number 5. Bridge abutments are to be set back 2m from top of waterway channel banks to facilitate green corridor and soft bank solution.

1.5m minimum maintenance headroom to underside of structure between beams. 0.9m minimum maintenance headroom to underside of discrete beams.

#### List of relevant documents from the TAS 4.2

See Appendix A

### 4.2.1 Additional relevant standards

BS 8500; Part 1; 2006 Concrete; Complementary British Standard to BS EN

206-1; Method of specifying and guidance for the

specifier

BS 8500; Part 2; 2006 Concrete; Complementary British Standard to BS EN

206-1; Specification for constituent materials and

concrete

CHE Memorandum 227/08 The Impregnation of Reinforced and Prestressed

Concrete Highway Structures using Hydrophobic Pore

Lining Impregnants

### 4.3 Proposed Departures from Standards given in 4.2 and 4.2.1

Implementation of CHE Memorandum 227/08 – Deletion of requirement for impregnation with hydrophobic pore lining Impregnants.

Modified longitudinal loading on Greenway structures – Deletion of BD37 requirements and provision for reduced alternative longitudinal load.

Application of combined waterproofing and surfacing to steel bridge decks – Use of proprietary anti slip coating system

Refer to Appendix E.

### 4.4 Proposed methods for dealing with aspects not covered by Standards in 4.2 and 4.2.1

None

### STRUCTURAL ANALYSIS

### 5.1 Methods of analysis proposed for superstructure, substructure and foundations

A static analysis approach will be used to calculate design loadings on superstructure, substructure and foundations.

The main longitudinal girders and cross-members will be analysed manually as simply supported line beams.

The stiffened steel decking will be analysed manually.

Abutments are to be analysed assuming vertical load carrying elements cantilever from pile caps.

Pile caps to be analysed assuming rigid pile caps and pinned connections between piles and pile caps.

Piles will be analysed and reinforced assuming a full moment connection with pile caps.

Wing walls will be analysed manually.

### 5.2 Description and diagram of idealised structure to be used for analysis.

See Appendix D

### 5.3 Assumptions intended for calculation of structural element stiffness

Element stiffness for steel members will be determined in accordance with BS 5400 Part 3:2000.

Element stiffness for concrete members will be derived in accordance with BS 5400 Part 4:1990 Clause 4.4, using full elastic uncracked member cross-sections ignoring the presence of reinforcement.

5.4 Proposed earth pressure coefficients ( k<sub>a</sub>, k<sub>0</sub>, or k<sub>p</sub> ) to be used in the design of earth retaining elements

For the analysis of the abutment and wing walls,  $k_a$  will be used for stability calculations and  $k_0$  for structural element design.

A representative peak angle of friction of  $35^{\circ}$  will be used for 6N/6P granular backfill, for which  $k_a = 0.27$ ,  $k_0 = 0.43$ , and  $k_p = 3.69$ .

Back of wall friction will not be considered.

Additional lateral loading on piles arising from residual approach embankment settlement will be analysed and added to pile loads arising from the deck and abutment analyses if appropriate.

### 6. GEOTECHNICAL CONDITIONS

6.1 Acceptance of recommendations of Section 8 of the Geotechnical Report to be used in the design and reasons for any proposed changes.

Section 2 of the Geotechnical Report has not been completed at this stage.

6.2 Geotechnical Report Highway Structure Summary Information (Form C)

A draft Geotechnical Report Highway Structure Summary sheet based on the information available in Part 1 of the Geotechnical Report is attached in Appendix C. A full Geotechnical Report Highway Structure Summary sheet and extracts from the completed Geotechnical Report Section 2 will be produced following development of the Geotechnical Report.

6.3 Differential settlement to be allowed for in the design of the structure.

The structure is founded on bored piles extending to the firm to very stiff Ashdown Formation. A maximum differential settlement of 10mm between abutments will be considered.

6.4 If the Geotechnical Report is not yet available, state when the results are expected and list the sources of information used to justify the preliminary choice of foundations.

The preliminary choice of foundation is discussed in the draft Geotechnical Report Highway Structure Summary sheet contained in Appendix C. Part 2 of the Geotechnical Report, including Section 2 Highway Structures, is expected to be completed in Phase 2 of the project.

### CHECKING

7.1 Proposed category of structure

Category 1 in accordance with BD2/05.

7.2 If Category 3, name of proposed Independent checkers.

N/A

7.3 Erection proposals or temporary works for which an independent check will be required, listing parts of the structure affected with reasons for recommending an independent check.

N/A

### 8. DRAWINGS AND DOCUMENTS

8.1 List of drawings and documents accompanying the submission.

Appendix A List of relevant documents from TAS dated February 2009

Appendix B Drawing No Title

The contraction of the contracti

B1297000-PH2/1600.01A/9191 Decoy Pond South Underbridge (G05)

Rev 0 General Arrangement

Appendix C Geotechnical Information

Appendix D Idealised Structure

Appendix E Departures from Standards

Date:

9	THE ABOVE IS SUBMITTED FOR ACCEP	TANCE
9.1	Submission by designer	
	Signed	
	Name: P. Blackie Position: Structures team leader, Jacobs Date: ไนโอคโเ2	Engineering Qualifications: BEng(Hons), CEng MICE
9.2	Endorsement by contractor	
	Signed	
	Name: S. LAPTHURN	Engineering Qualifications: Many (Hons) Cong MICE.
	Position: Design Coordinator	Hochtief Vinci Joint Venture
	Date: 20/09/12	
10.	THE ABOVE IS REJECTED/AGREED SUE SHOWN BELOW.	BJECT TO THE AMENDMENTS AND CONDITIONS
	Reviewed:	
	Name:	Engineering qualifications:
	Date:	
	Signed:	
	Name: TAA	Engineering qualifications:

额

Doc. Ref: B1297000-PH2/1600.01A/0021 Rev 0





## Appendix A List of Relevant Documents

Schedule of Design Documents Relating to Highway Bridges and Structures; February 2009

### **British Standards**

BS 5268; Part 2; 2002	Structural Use of Timber				
BS 5400	Steel concrete and composite bridges				
Part 1; 1988	General Statement (see BD 15 )				
Part 2; 1978	Specification for loads (see BD 37)				
Part 3; 2000	CP for design of steel bridges (see BD 13)				
Part 4; 1990	CP for design of concrete bridges (see BD 24)				
Part 5; 1979	CP for design of composite bridges (see BD 16)				
Part 9; 1983	Bridge bearings (see BD 20)				
Part 10; 1980	CP for fatigue (see BD 9)				
BS 5628; Part 1; 1992	Unreinforced Masonry				
BS 5930; 1999	Site Investigations				
BS 6031; 1981	Earthworks				
BS 8002; 1994	Earth retaining structures				
BS 8004; 1986	Foundations				
BS-8118; 1991	The structural use of aluminium				
BS EN 1317-1-1998; Road Restraint Systems – Part 1	Terminology and general criteria for test methods				
BS EN 1317-2-1998; Road Restraint Systems – Part 2	Performance classes, impact test acceptance criteria and test methods for safety barriers				
BS EN 1317-3-2000; Road Restraint Systems - Part 3	Performance classes, impact test acceptance criteria and test methods for crash-cushions				
DD-ENV-1317-4-2002; Road Restraint Systems Part 4	Terminals and transitions				
BS-EN-14388; 2005	Road traffic noise reducing devices - Specification				

### Miscellaneous

Circular Roads No 61/72 - Routes for heavy and high abnormal loads.

Railway Group Approved Code of Practice GC/RC5510: Recommendations for the Design of Bridges (2000) (for full-list of other Network Rail Standards, refer to RSSB, Railway Safety and Standards Board)

Simplified Tables of External Loads on Buried Pipelines (1986)

Traffic Management Act 2004

### The Manual of Contract Documents for Highway Works (MCDHW)

Volume 1: Specification for Highway Works 1998, including amendments to May 2009

Volume 2: Notes for Guidance on the Specification for Highway Works 1998, including amendments to

May 2009

Volume 3: Highway Construction Details 1991, including amendments to November 2008

### The Design Manual for Roads and Bridges (DMRB)

Bridges and Structures ( BA Series )

Reproduced on following pages

Bridges and Structures (BD Series)

Reproduced on following pages

Bridges and Structures, Technical Memoranda (BE Series)

Reproduced on following pages

### Traffic Engineering and Control, Standards (TD Series)

TD 9/93 Road layout and geometry. Highway link design

TD 19/06 Requirement of Road Restraint Systems & correction No. 1

TD 27/05 Cross Sections and headroom

TD 36/93 Subways for pedestrians and cyclists, layout and dimensions

### Highways, Advice Notes (HA Series)

HA 59/92 Mitigating Against Effects on Badgers

HA 80/99 Nature Conservation Advice in Relation to Bats

HA 84/01 (1) Nature Conservation and Biodiversity

HA 97/01 Nature Conservation Management Advice in Relation to Dormice

HA 98/01 Nature Conservation Management Advice in Relation to Amphibians

### Highways, Standards (HD Series)

HD 22/08 Managing Geotechnical Risk

	ADVICE NOTES - BRIDGES AND STRUCTURES (BA SERIES)
BA-9/81	The Use of BS 5400: Part 10: 1980. Code of Practice for Fatigue Amendment No. 1
BA 16/97	The Assessment of Highway Bridges and Structures.  Amendment No. 1  Amendment No.2
BA 19/85	The Use of BS 5400: Part 3: 1982
BA 24/87	Early Thermal Cracking of Concrete Amendment No. 1
BA 26/94	Expansion Joints for Use in Highway Bridge Decks
BA 28/92	Evaluation of Maintenance Costs in Comparing Alternative Designs for Highway Structures
BA-30/94	Strengthening of Concrete Highway-Structures Using Externally Bonded Plates
BA 34/90	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures
BA-35/90	Inspection and Repair of Concrete Highway Structures
BA-36/90	The Use of Permanent Formwork
BA-37/92	Priority Ranking of Existing Parapets
BA 38/93	Assessment of the Fatigue Life of Corroded or Damaged Reinforcing Bars
BA-39/93	Assessment of Reinforced Concrete Half-joints
BA-40/93	Tack-Welding of Reinforcing Bars
BA 41/98	The Design and Appearance of Bridges
BA-42/96	The Design of Integral Bridges [Incorporating Amendment No. 1 dated May 2003]
BA-43/94	Strengthening, Repair and Monitoring of Post-tensioned Concrete Bridge Decks
BA-44/96	Assessment of Concrete Highway Bridge and Structures
BA 47/99	Waterproofing and Surfacing Concrete Bridge Decks
BA 50/93	Post-tensioned Concrete Bridges: Planning, Organisation and Methods for Carrying Out Special Inspections
BA 51/95	The Assessment of Concrete Structures Affected by Steel Corrosion
BA 52/94	The Assessment of Concrete Highway Structures Affected by Alkali Silica Reaction
BA 53/94	Bracing Systems and the Use of U-Frames in Steel Highway Bridges
BA 54/94	Load Testing for Bridge Assessment
BA-55/06	The Assessment of Bridge Substructures and Foundations, Retaining Walls and Buried Structures
BA 56/96	The Assessment of Steel Highway Bridges and Structures
BA 57/01	Design for Durability
BA-58/94	Design of Bridges and Concrete Structures with External Unbonded Prestressing
BA 59/94	Design of Highway Bridges for Hydraulic Action
BA-61/96	The Assessment of Composite Highway Bridges
BA-67/96	Enclosure of Bridges
BA 68/97	Crib Retaining Walls

	ADVICE NOTES - BRIDGES AND STRUCTURES (BA SERIES)
BA 72/03	Maintenance of Road Tunnels
BA-74/06	Assessment of Scour at Highway Bridges
BA-80/99	Use of Rock Bolts
BA-82/00	Formation of Continuity Joints in Bridge Decks
BA-83/02	Cathodic Protection for Use in Reinforced Concrete Highway Structures
BA 84/02	Use of Stainless Steel Reinforcement in Highway Structures
BA 85/04	Coatings for Concrete Highway Structures & Ancillary Structures
BA-86//06	Advice Notes on the Non-Destructive Testing of Highway Structures
BA-87//04	Management of Corrugated Steel Buried Structures
BA-88//04	Management of Buried Concrete Box Structures
BA 92/07	The Use of Recycled Concrete Aggregates in Structural Concrete
BA-93/09	Structural Assessment of Bridges with Deck Hinges
	STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)
BD 2/05	Technical Approval of Highway Structures
BD 7/01	Weathering Steel for Highway Structures
BD 9/81	Implementation of BS 5400: Part 10: 1980. Code of Practice for Fatigue
BD 10/97	Design of Highway-Structures in Areas of Mining Subsidence
BD-12/01	Design of Corrugated Steel Buried Structures with Spans Greater than 0.9 Metres and up to 8.0 Metres
BD 13/06	Design of Steel Bridges. Use of BS 5400: Part 3: 2000
BD 15/92	General Principles for the Design and Construction of Bridges. Use of BS 5400: Part 1: 1988
BD-16/82	Design-of-Composite-Bridges. Use of BS-5400: Part 5: 1979 Amendment No. 1
BD 20/92	Bridge Bearings. Use of BS 5400: Part 9: 1983
BD 21/01	The Assessment of Highway Bridges and Structures
BD 24/92	Design of Concrete Bridges. Use of BS 5400: Part 4: 1990
BD-27/86	Materials for the Repair of Concrete Highway Structures
BD 28/87	Early Thermal Cracking of Concrete Amendment No. 1
BD 29/04	Design Criteria for Footbridges
BD 30/87	Backfilled Retaining Walls and Bridge Abutments
BD 31/01	The Design of Buried Concrete Box and Portal Frame Structures
BD 33/94	Expansion Joints for Use in Highway Bridge Decks
BD-34/90	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures
BD 35/06	Quality Assurance Scheme for Paints and Similar Protective Coatings
BD 36/92	Evaluation of Maintenance Costs in Comparing Alternative Designs for Highway

	STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)
	Structures
BD 37/01	Loads for Highway Bridges
BD-41/97	Reinforced Clay Brickwork Retaining Walls of Pocket Type and Grouted Cavity type Construction Use of BS 5628: Part 2: 1995
BD-42/00	Design of Embedded Retaining Walls and Bridge Abutments
BD-43/03	The Impregnation of Reinforced and Prestressed Concrete Highway Structures using Hydrophobic Pore-Lining Impregnants
BD-44/95	The Assessment of Concrete Highway Bridges and Structures
BD 45/93	Identification Marking of Highway Structures
BD 46/92	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures [Stage 2 - Modern Short Span-Bridges]
BD-47/99	Waterproofing and Surfacing of Concrete Bridge Decks
BD 48/93	The Assessment and Strengthening of Highway Bridge Supports
BD 49/01	Design Rules for Aerodynamic Effects on Bridges
BD-50/92	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures Stage 3 - Long Span Bridges
BD 51/98	Portal and Cantilever Signs/Signal Gantries
BD 53/95	Inspection and Records for Road Tunnels
BD-54/93	Post-tensioned Concrete Bridges, Prioritisation of Special Inspections
BD 56/96	The Assessment of Steel Highway Bridges and Structures
BD 57/01	Design for Durability
BD 58/94	The Design of Concrete Highway Bridges and Structures with External and Unbonded Prestressing Design of Highway Bridges for Vehicle Collision Loads
BD-60/04	Design of Highway Bridges for Vehicle Collision Loads
BD-61/96	The Assessment of Composite Highway Bridges
BD 62/07	As Built, Operational and Maintenance Records for Highway Structures
BD 63/07	Inspection of Highway Structures
BD 65/97	Design Criteria for Collision Protector Beams
BD-67/96	Enclosure of Bridges
BD-68/97	Crib-Retaining Walls
BD-70/03	Strengthened/Reinforced Soils and Other Fills for Retaining Walls and Bridge Abutments Use of BS8006: 1995, incorporating Amendment No. 1 (Issue 2 March 1999)
BD 74/00	Foundations
BD-78/99	Design of Road Tunnels
BD 79/06	The Management of sub Standard Highway Structures
BD-81/02	Use of Compressive Membrane Action in Bridge Decks
BD-82/00	Design of Buried Rigid Pipes
BD 84/02	Strengthening of Concrete Bridge Supports Vehicle Impact Using Fibre Reinforced Polymers
BD-85/08	Strengthening Highway Structures Using Externally Bonded Fibre Reinforced Polymer

	STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)
BD-86/07	The Assessment of Highway Bridges and Structures For The Effects of Special Types
BB 00/07	General Order (STGO) and Special Order (SO) Vehicles
BD-87/05	Maintenance Painting of Steelwork
BD-89/03	The Conservation of Highway Structures
BD-90/05	Design of FRP Bridges and Highway Structures
BD-91/04	Unreinforced Masonry Arch Bridges
BD-94/07	Design of Minor Structures
BD-95/07	Treatment of Existing Structures on Highway-widening Schemes
	TECHNICAL MEMORANDA - BRIDGES (BE SERIES)
BE-13	Fatigue Risk in Bailey Bridges
BE-23	Shear Key Decks Amendment No. 1 to Annex
BE 5/75	Rules-for-the-Design-and-Use of Freyssinet-Concrete-Hinges-in-Highway-Structures
BE-7/04	Departmental Standard (Interim) Motorway Sign/Signal Gantries
	INTERIM ADVICE NOTES (IAN)
IAN 117/08 Rev 1	Certification of combined kerb and drainage products
IAN-116/08	Nature conservation advice in relation to bats
IAN 104/07	The Anchorage of Reinforcement and Fixings in Hardened Concrete
IAN-97/07	Assessment and upgrading of existing parapets
IAN-96/07r1	Guidance on implementing Results of Research on Bridge Deck Waterproofing
IAN 95/07	Revised Guidance Regarding the Use of BS8500(2006) For the Design and Construction of Structures Using Concrete
IAN-91/07	Interim Advice on the identification of "Particularly at Risk" supports
IAN 70/06	Implementation of New Reinforcement Standards
IAN 69/05	Design for Maintenance
IAN 48/03	Measures To Minimise The Risk of Sulphate Attack (Including Thaumasite) - New Construction and Structures Under Construction
IAN 47/02	Post Tensioned Grouted Duct concrete Bridges
IAN 41/02	European Cement Standards
1441.00/00	
IAN 05/96	BD 24/92 The Design of Concrete Highway Bridges and Structures. Use of BS 5400: Part 4:1990

BA 50/93 Post Tensioned concrete Bridges

IAN 03/96

## Appendix B Drawings

Drawing No

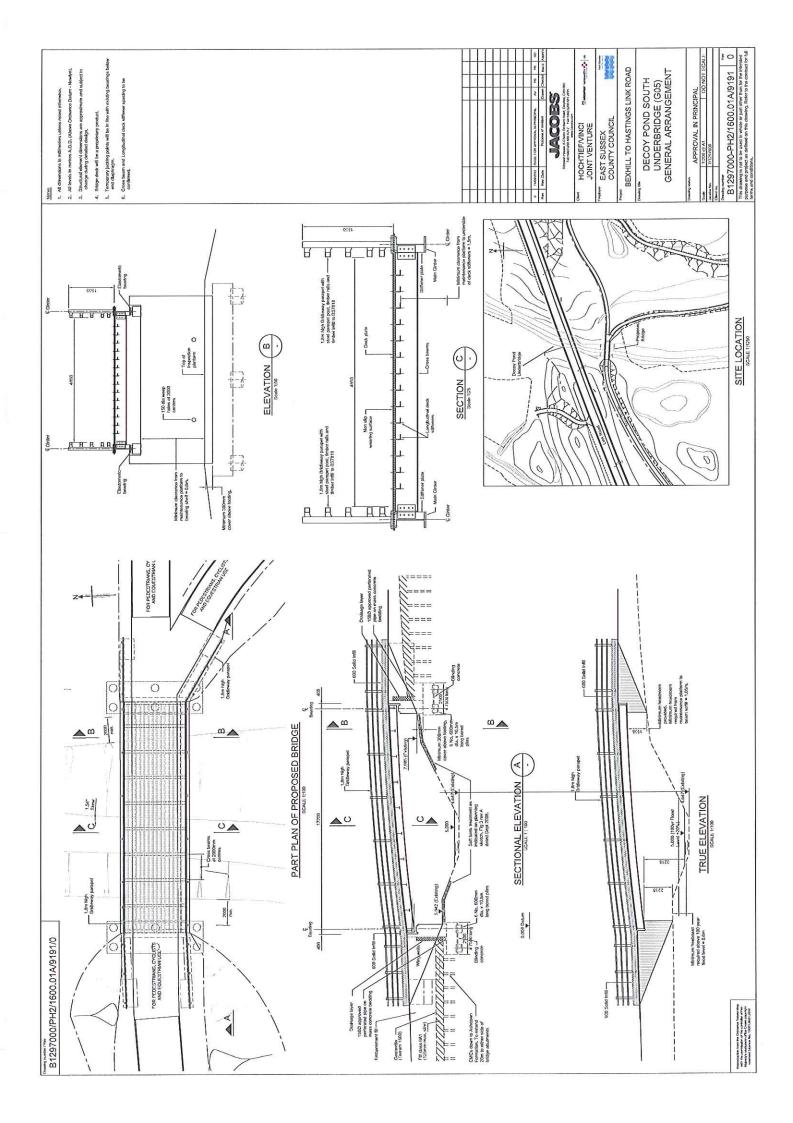
Title

B1297000-PH2/1600.01A/9191

Decoy Pond South Underbridge (G05) General

Arrangement

		*	





## Appendix C Geotechnical Information

Doc. Ref: B1297000-PH2/1600.06A/0021 Rev 0

### BEXHILL TO HASTINGS LINK ROAD

### **GEOTECHICAL SUMMARY INFORMATION**

STRUCTURE NA	ME	CHAINAGE and OS Grid Reference			
G05 - Decoy Pon	d South UB	Ch 4840 OS: 576765.720E, 110826.243N			
		DESIGN LIFE: 120 years			
SOILS/GEOLOG	Υ	RELEVANT EXP	LORA	ATORY	HOLES:
		BH195, BH196, 0	CPT7	(URS In	vestigation, 2009)
Strata				Typica	l depths
<u>West</u>					
Alluvium				5.62 to	3m OD
Ashdown Format	ion – interbedde	ed sands, silts and	clay	Below	3m OD
<u>East</u>					
Alluvium				8.38 to	5.3m OD
Ashdown Format	ion – interbedde	ed sands, silts and	clay	Below 5.3m OD	
PREVIOUS GRO	UND	Agricultural land			
CONTAMINATED REQUIRED	O GROUND RIS	K ASSESSMENT	9	No	
GROUNDWATER	२				
Groundwater was encountered in BH195 initially at 2.62m OD (3m bgl) within the Ashdown Formation and rose to a level of 2.92m OD (2.7m bgl) in 20 minutes. A second groundwater strike encountered confined groundwater within Ashdown Formation at 0.22m OD (5.4m bgl) and rose to a level of 4.62m OD (1m bgl) in 20 minutes. Groundwater monitoring carried out between February 2009 and March 2010 indicates a level of up to 0.27m bgl  Allowing for seasonal fluctuations, the preliminary design groundwater level is assumed at ground level.					
EARTH PRESSURE VALUE K <sub>0</sub> * K <sub>a</sub> * Kp*					
Refer to Section 5	5.4 of the AIP.				
TYPE OF FOUNDATION	Piled foundation	on			
BEARING CAPACITY	N/A				

Structure Element	Founding Stratum	Foundir Level (m AOD		Footing Size	Allowable Bearing Pressure (kN/m2)
PILE DESIGN					
Structure Element	Founding Stratum	Toe Level (mAOD)	Pile dia (m)	Pile length (m)	Pile working Load (kN)
West Abutment	Ashdown Formation Ashdown	-5.66	0.6	10.5	350
East Abutment	Formation	-3.82	0.6	10.5	350
					×.

Note: Pile lengths and toe levels are approximate – pile cap elevations to be confirmed.

Pile type: Bored / CFA

Criteria for selecting pile toe level: Allowable pile capacity

Allowance for negative skin friction within design: Negative skin friction considered

### SETTLEMENT

Differential settlement to be allowed for between adjacent supports: 10mm

Differential settlement to be allowed between structure and approach embankment: 20mm (within 10 metres of the interface between structures and approach embankments)

### CHEMICAL ANALYSIS

### **Buried Concrete classification:**

The results of chemical tests on soil samples taken within the rural areas indicate pH values ranging between 3.8 to 9.4 and sulfates (2:1 Water Extract) values of between 10 to 900mg/l. The recommended Design Sulfate and Concrete Classification based on BRE Special Digest 1 (2005) are DS-2 and AC-3z respectively.

### NOTES

- 1. The ground conditions at the site comprise Alluvium overlying Ashdown Beds. Alluvium is not recommended as a bearing stratum due to its unpredictable bearing behaviour and poses a risk of differential settlement taking place. The maximum thickness of Alluvium is 2.3m.
- 2. It is recommended that the foundation of the structure is founded on the firm to very stiff Ashdown Formation at minimum levels of 3m OD (aprox 2.5m bgl) for West Abutment and 5.3m OD (aprox 3m bgl) for East Abutment. Due to the likely depth of excavation at this stage, it is proposed to consider using piled foundations.
- 3. The behaviour of the groundwater indicates likely presence of confined aquifer. This should be considered during construction.

Doc. Ref: B1297000-PH2/1600.06A/0021 Rev 0

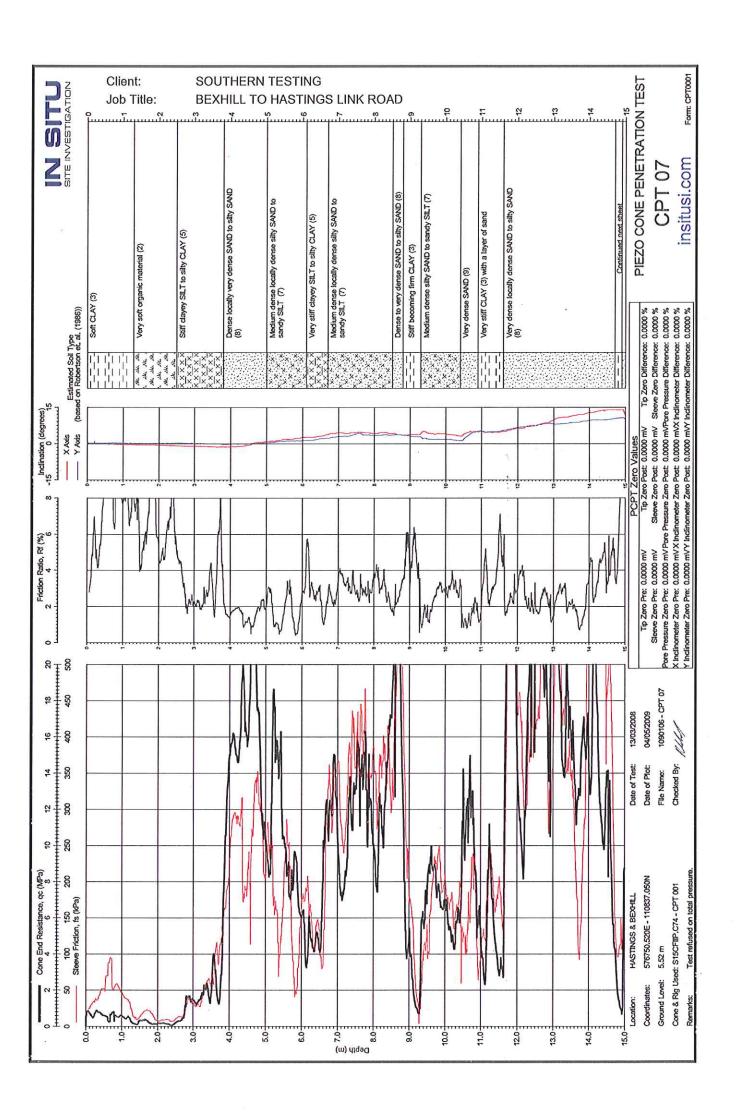
20.00	Contrac	ct No: 49	9325727					TURS	
The state of the state of	Project	В	exhill - Hastin	gs L	ink R	oad		Record of Borehol	le
	Client:	E	ast Sussex Co	oun	ty Cou	ıncil		BH195	
	SAMP	LES &	In situ TESTS	L				STRATA	
-	Depth	Type/ No.	SPT/U4 (Blows)	Water	Reduced Level (mOD)	Legend	Depth (Thick- ness)	DESCRIPTION	ment/
				1	5.42	111511	0.20	TOPSOIL	
	0.50	D1		.a. ∑_				Soft brown mottled dark orange-brown and grey slightly sandy CLAY with rare gravel sized pockets of white clay. Sand is fine. Occasional fine rootlets. (Zone V) (ALLUVIUM)	
	1.00	D2		Δ̈́	4.62		_1.00	Soft extremely to very closely fissured light brown, orange-brown and light grey mottled CLAY, (Zone V) (ALLUVIUM)	
	2.00	U3 D4	(10 - 450mm)		3.92	<u></u>	_1.70 - -	Soft light and dark grey slightly peaty slightly sandy silty CLAY with rare lithorelics of very weak dark grey angular fine to medium siltstone. Organic matter is pseudo-fibrous and slightly spongy. (Zone IV) (ALLUVIUM)	
The second second second	2.50	U5	(20 - 450mm)	Ţ	3.12	/	2.50	Stiff light blue-grey and orange-brown mottled black slightly clayey SILT. (ASHDOWN BEDS)	
	3.00	D6 W7 SPT8	N=17 (3/5/4/4/5/4)	*		× × × × × × × × × × × × × × × × × × ×	(1.00)	From 3.0m bgl with frequent horizontally aligned lithorelics of very weak blue-grey and orange-brown stained orange brown angular to subangular fine to medium siltstone. (Zone III)	
	3.50	U B9	(56 - 0mm)		2.12	X X X X X X X X X X X X X X X X X X X	(1.00)	Between 3.5m bgl to 3.45m bgl becoming light yellow-brown, slightly light blue-grey and orange-brown colour banded mottled black stained orange-brown sandy SILT. Sand is fine.  Yellow-brown slightly light blue-grey and orange-brown colour banded slightly sandy SILT interbedded with SILTSTONE. discontinuities appear to be extremely to closely spaced. (Zone III to II) (Recovered as very weak orange-brown and light grey stained orange-brown angular to subangular fine to coarse gravel and cobble and siltstone.) (ASHDOWN BEDS)	
A PART INTO THE PART INTO	4.50	SPT10	N=13 (3/3/3/3/3/4)		1.12		4.50	Firm dark brown and grey mottled black slightly clayey SILT with occasional lithorelics of very weak black and dark orange-brown subangular fine to coarse siltstone (possible interbedded with siltstone bands). (Zone III to II) (ASHDOWN BEDS)	
	5.40 5.50	D11 W12 SPT13	N=49 (3/4/5/8/17/19)	**	_0.22 0.08	X X X X X X X X X X X X X X X X X X X	5.70	Weak dark grey-dark brown and dark orange-brown occasionally thinly laminated (<1mm) black and light grey-white stained dark orange-brown slightly weathered SILTSTONE. Discontinuities appear to be very closely to closely spaced. (Zone II) (Recovered as flat/columnar subangular to sub-rounded medium to coarse slightly sitly gravel and cobble of silistone.) (ASHDOWN BEDS)  Wery stiff dark grey and dark orange-brown stained orange-brown SILT. (Zone	
	6.50	SPT14	N=36 (4/6/6/7/6/17)			× × × × × × × × × × × × × × × × × × ×		(ASHDOWN BEDS)  Weak dark grey-dark brown and dark grange-brown, stained dark grange	
The state of the s	7.50	D15	N=58		-1.48	* * * * * * * * * * * * * * * * * * *	7.10	Weak dark grey-dark brown and dark orange-brown stained dark orange brown slightly weathered SILTSTONE, Discontinuities appear to be very closely spaced. (Zone II) (Recovered as flat subangular to sub-rounded medium to coarse slightly silty gravel of siltstone.)  (ASHDOWN BEDS)	
	<i>t.</i> au l		g Progress and '	Wate	er Obse		ns	Chiselling Water Added GENERAL	
	Date	Time	Hole Cas'g Cas'g	Wa	ter Ros	e Tim	e Sealed		

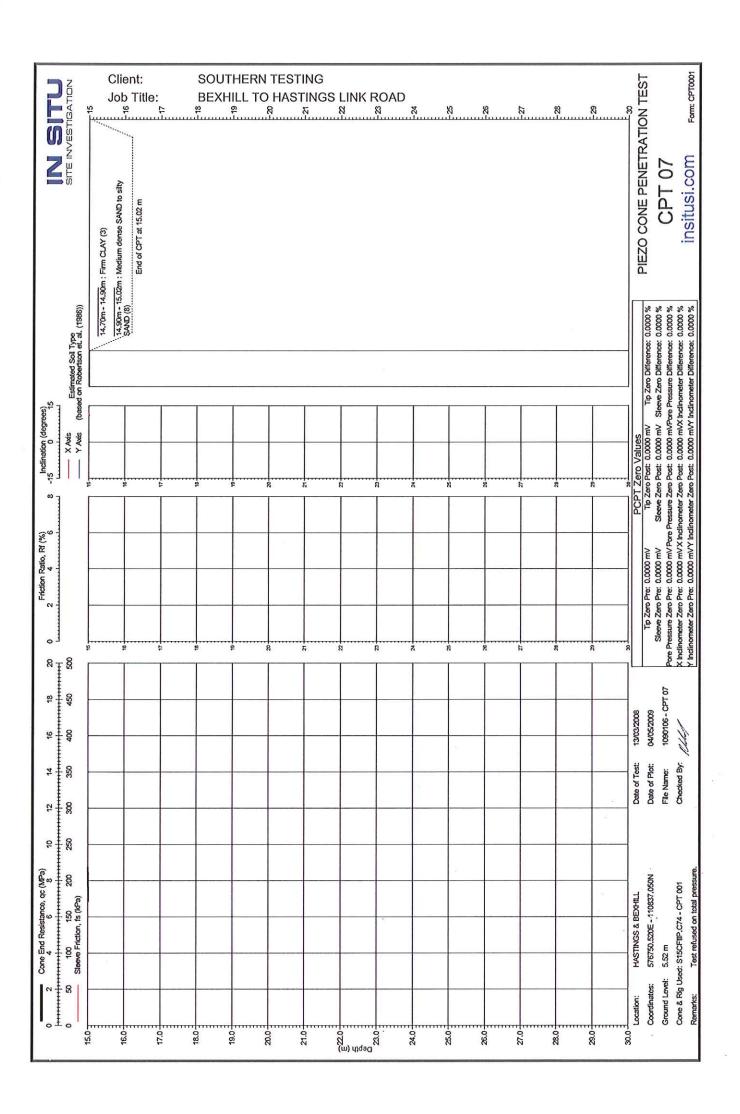
7.50	SPT16		N=58			×	×								V////
	Borir	ng Pro	gress	and V	Vater	Observ	vations	3	Chiselling			Water Added		GENERAL	
Date	Time	Hole Depth	Cas'g Depth	Cas'g Dia	Water Depth	Rose	Time (mins)	Sealed (m)	From	То	Time (hh:mm)	From	То		REMARKS
10/02/09 10/02/09		3.00 5.40	2.50 4.00	150 150	3.00 5.40	2.65 1.00	20 20	()	7.00	7.10	00:15			Draft During logging no visible or olfactory evidence of contaminat Zone of weathering interpreted fr from Spinks et al. 1993: (V); (iV) (III); (II);(I).	
Logged by: JB Checked by CAB Status: Draft		Contra	Percus		g - Dano boratorio	l do 2000 es Ltd			: 16.3 E 10.2 N		Ground L 5.62 mAOD	evel:	Date: 10/02/200 10/02/200		Scale: 1:40.0 Sheet 1 of 2

14/06/2009 12:34:51	Contra	ct No: ∠	1932	5727													TUR	S
ted: 14/09/20	Project: Bexhill - Hastings Link Road													Record of Borehole				
ALLGPJ Pri	Client: East Sussex County Council  SAMPLES & In situ TESTS  STRATA														BH19	5		
SS	SAME	PLES	& In	situ Ti	ESTS	L.							STR/	ATA				
SAM: BEXHILL BORGHOLE LOG FIM: J'BEDRORD-LOBSIE/AST GUSSEX COUNTY COUNCILMIZE/TZ BEXHILL TO HASTNIGS LINK ROADITECHNICALIFACTUAL REPORT DATAGNITBEDHILL - MASTNIGS	Depth	Type/ No.		SPT/U (Blows		Water	Reduce Level (mOD)	Legen	d	Depth (Thick- ness)				DESC	RIPTION			Instru- ment/
XJEL			(10/15	5/55mm/13/	13/12/20			-× × × ×	×	-								
T DATAK							-2.38	×××	1	8.00								
REPOR								× × ×	×	:-	Stiff to ve orange b	ery stiff da rown cold k SII TST	ark grey, gre our laminate ONE recov	ey and da ed orange vered as o	rk brownish brown stair occasional li	grey occas ned SILT in thorelics of	sionally thickly terbedded with very weak to one. (Zone III to	
FACTUA								× ×	,	4	II)			subangula	r fine to me	dium siltsto	ne. (Zone III to	
HNICAL	8.50	SPT17		N=24 (3/6/6/6/6	/6)			× ×	X	-	(ÁSHDO	MN RED	S)					
DADITEC								* * ×	k	(2.00)								
S LINK R	9.00	D18						* × ×	,									
HASTING								]× × ×	*	]								
HEL TO	9.50	SPT19		N=43 5/8/10/10/1	1/12)		,	× ×	*	-								
727 BEX					5			-× ×	1									
CILM932						┢	-4.38	x x	+	10.00			Fud	of Dorol	ala at 40.0	٥		
YCOUN													End	of Borer	ole at 10.0	UIII		
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GSSns.									1									
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S JABEDI																		
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Lid Horne Lane Bedford MK40 1TS Telephone: 01224 349641 www.URSCorp.com		Borin		gress							С	hiselli		Water	Added	1	GENERAL	
9: 01234	Date	Time	Hole Depth	Cas'g Depth	Cas'g Dia	Wat Dep	ter Ros		ne ns)	Sealed (m)	From	То	Time (hh:mm)	From	То	Droft	REMARKS	f
Telephon	0/02/09	16.30	10.00	7.00	150	1.0			,	, , , ,						During log	gging no visible or svidence of contam eathering interprete ks et al. 1993: (V);	ination.
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ane lane																		
LIGHTON.	ogged by:		Equip					20		Location			Ground L	500,000,000,000	Date:	0.01	Scale:	
pormition	hecked by	r.	Cable	Percuss	sion Ri	9 - Da	ando 20	JU	$\dashv$		16.3 E		5.62 mAOD	- 1	10/02/200 10/02/200		1:40.0	
8	tatus: Oraft			ern Test	ing Lat	orate	ories Ltd			1108	10.2 N		IIIAOD		, O/OZ/ZOU	o End	Sheet 2 of 2	

Contra	ct No: ∠	19325	5727						TIRS	2		
Project	Project: Bexhill - Hastings Link Road											
Client:	BH196	3										
SAME	PLES	& In s	situ TE		1				STRATA			
Depth	Type, No.		SPT/U- (Blows		Water	Reduced Level (mOD)	Legend	Depth (Thick- ness)	DESCRIPTION	ment/ Backfill		
0.50	D1							(1.00)	Soft, medium brown CLAY, with occasional fine rootlets and fine to medium, angular, randomly orientated lithorelics of orange/brown mudstone.  (TOPSOIL)			
1.00	D2		822 DEG	61		7.38		1.00	Soft, medium brown and grey brown mottled CLAY, with rare, coarse roots and fine, randomly orientated lithorelics of weak, brown mudstone.  (ALLUVIUM)			
2.00	U3 D4		(20 - 450m	m)		_6.68	  -  -	1.70	Soft, very closely fissured, brown and light grey mottled SILT/CLAY, with frequent lithorelics of randomly orientated, coarse, very weak, orange/brown siltstone. Frequent, heavy, dark orange iron staining present along fissures. (ASHDOWN BEDS)			
2.50	U5		(70 - 360m	m)				-				
3.00	D6 SPT7		N=20 (2/3/3/4/5/	8)		5.38	× × × × × × × × × × × × × × ×	3.00	Poor recovery, recovered as stiff, orange/brown and grey mottled SILT, with frequent fine to coarse, angular gravels of siltstone. Siltstone is weak, thinly colour banded orange/brown and light grey.  (ASHDOWN BEDS)			
3,50	U8	1	(80 - 360m	m)			× × × × × × × × × × × × × × × × × × ×	(1.00)				
4.00	D9					4.38	× × × × × × × × × × × × × × × × × × ×	(1.00)	Firm, thickly colour laminated, grey and orange/brown SILT, with frequent, horizontally aligned lithorelics of medium to coarse siltstone, Frequent heavy iron staining present along faces of lithorelics.  (ASHDOWN BEDS)			
4.50	U10	(	100 - 300m	ım)			× × × × × × × × × × × × × × × × × × ×		-			
5.00	D11 SPT12	(5/	N=46 10/11/11/1	1/13)		3.38	X X X X X X X X X X X X X X X	5.00	Very weak, grey SILTSTONE recovered as grey silt, with frequent fine to medium, angular to sub-angular gravels of siltstone. (ASHDOWN BEDS)			
5.50	D13 U14	1	(45 - 450mi	n)		2.88		5.50	Stiff, very closely fissured, grey/brown and orange/brown mottled CLAY with occasional fine to medium, very stiff, orange/brown lithorelics. Occasional dark brown/black silt and heavy, dark orange iron staining present along fassures.  (ASHDOWN BEDS)			
6.00	D15					-2.30		(1.00)	Stiff, very closely fissured, light grey, yellow/brown and bright orange mottled CLAY, with rare, fine to coarse, honzontally aligned, dark orange lithorelics of weak mudstone.  (ASHDOWN BEDS)			
6.50	U B16		(100 - 0mn	1)		1.38		7.00				
7.00	SPT17	(25/4	N=>60 40/60/70mr	n/-/-/-)		0.98	X	7.40	Very poor recovery; weak SILTSTONE recovered as loose, light grey silt. (ASHDOWN BEDS)			
7.40	SPT18		N=>100 nm/-/60/40/-	40mm/-/-)					End of Borehole at 7,40m			
Data		ng Pro Hole	Cas'g					Sealed	Chiselling Water Added GENERAL  GENERAL  REMARKS			
Date	Time	Depth	Depth	Dia	Dep	oth to	(mins		From To (hh:mm) From To	m. nation. and d from V);		

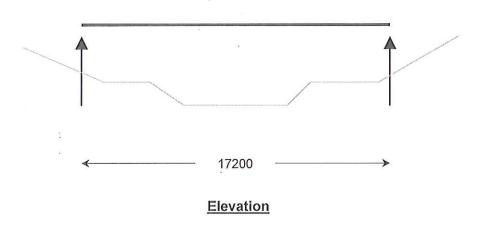
				(III); (II);	nks et al. 1993: ( l).
Logged by: HH Checked by:	Equipment: Cable Percussion Rig - Dando 2000	Location: 576778.0 E	Ground Level: 8.38	Date: 30/01/2009 Start	Scale: 1:40.0
CAB Status:	Contractor: Southern Testing Laboratories Ltd	110819.1 N	mAOD	30/01/2009 End	Sheet 1 of 1

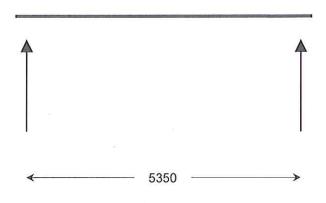




## Appendix D Idealised Structure

### DIAGRAM OF IDEALISED STRUCTURE TO BE USED IN ANALYSIS





**Sectional View** 

### Appendix E Departures from Standards

### Departure # Hydrophobic Pore Lining Impregnant

BD 43/03 specifies various requirements for the impregnation of highway structures with hydrophobic pore lining impregnant. Following the completion of research into the long term effectiveness of hydrophobic pore lining impregnants on concrete highway structures, the Highways Agency is temporarily suspending requirements to apply all such impregnants as set out in BD43/03.

This suspension is detailed in CHE Memorandum 227/08 - The Impregnation Of Reinforced and Prestressed Concrete Highway Structures Using Hydrophobic Pore Lining Impregnants

This Departure seeks to apply this suspension to structures on the BHLR – i.e. the impregnant will not be applied.

This will not preclude the opportunity to apply impregnant in the future should this be required.

### Departure # Longitudinal Loading on Greenway Structures

This Departure seeks approval:

- to delete the BD37/01 Clauses 6.10 and 6.11 requirements for longitudinal load for traction and braking and accidental load due to skidding.
- to apply instead a single alternative nominal longitudinal load of 150 kN. This load will be applied as described in BD37/01 Clause 6.10

The BD37 requirements for these loadings are based on significantly higher traffic loads and speeds than the Greenway structures will be subjected to. The 150 kN proposed is based on the maximum horizontal load that can be generated by the 24 tonne design vehicle reacting on the structure with a coefficient of friction of 0.6 between vehicle and deck. We consider that this approach is moderately conservative and appropriate to the structures concerned.

### Departure # Combined Waterproofing and Surfacing on Steel Bridge Decks

This departure seeks approval for use of proprietary product for waterproofing and anti slip treatment of the steel bridge decks. This is required as waterproofing and corrosion protection of steel bridge decks is not covered in Clause 1802 - surface preparation and protection against corrosion – Specification, Structures SHW, MCHW Vol 1, Series 1800 – Structural Steelwork.

It is proposed to use a resin based system with a slip resistant aggregate dressing e.g. Bimagrip or CICOL.

Use of such products is typical on steel footbridges and link span bridges and is recommended for use on equestrian bridges by the British Horse Society.

